The Arm Equation and Reliability of 6-DOF KUKA Robot

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Abstract

In this paper the arm equation of 6-axes articulated KUKA robot [KR-16] is derived using Denavit-Hartenberg algorithm. Given an explicit task to be executed, a robot might be used to find the probability of success or reliability. Here, an experimental set up has been established and reliability is evaluated from experimental data. Moreover, a relationship between reliability and repeatability of robot is established.

Keywords: Forward Kinematics, KUKA Robot, Reliability.

I. Introduction

In order to benefit from robotic technology, reliability should be considered a major portion of investment decisions. Robotic systems are complex. Thus uncertainty cannot be avoided. The reliability of robot can be found by either of the following methods:

- 1. In terms of previous failure data of robot.
- 2. In terms of component of the robot.
- 3. In terms of the performance of the robot.

In this paper, we have found out reliability of the robot in terms of its performance.

In this paper the kinematics modeling of KR-16 KUKA robot as shown in Fig.1 is carried out and reliability is found experimentally. The various dimensions of KR-16 robot is shown in Fig.2. Generally, KUKA Robotics is a leading German producer of industrial robots for a variety of industrial processes like welding, painting etc. The robotic arm comes with a control panel that has a display and an integrated mouse, with which the manipulator is moved, positions are saved, or where modules, functions, and data lists are created and modified. Controls for the latest control panel use the Windows XP operating system. The KR-16 is a 6-axes robotic arm weighting 235 kg with the payload up-to 16 kg. [11].

II. The Arm Equation

Using DH algorithm, the different frames are developed in Figures 3 (a), (b), (c), (d), (e), (f) and (g) and kinematic table showing different parameters is prepared [9]. The kinematic table of 6-axes robot is shown in Table1:

Table1: Kinematic Table

i	θ	d	a	α
1	q_1	675mm	260 mm	-90°
2	$q_2 - 90^0$	0mm	680 mm	0^0
3	q ₃	0mm	0 mm	90^{0}
4	q_4	-670mm	0 mm	-90°
5	q ₅	0 mm	0 mm	90^{0}
6	q_6	-158 mm	0 mm	180^{0}

The arm equation is then derived as follows:

 $\mathbf{T} = \mathbf{T}_0^1 \mathbf{T}_1^2 \mathbf{T}_2^3 \mathbf{T}_3^4 \mathbf{T}_4^5 \mathbf{T}_5^6$

Where general forms of T_{k-1}^k is given as

$$T_{k-1}^{k} = \begin{bmatrix} C\theta_{k} & -C\alpha_{k}S\theta_{k} & S\alpha_{k}S\theta_{k} & a_{k}C\theta_{k} \\ S\theta_{k} & C\alpha_{k}C\theta_{k} & -S\alpha_{k}C\theta_{k} & a_{k}S\theta_{k} \\ 0 & S\alpha_{k} & C\alpha_{k} & d_{k} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

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So, first we determine

$$\begin{split} \mathbf{T}_{0}^{1} &= \begin{bmatrix} \mathbf{C}_{1} & 0 & -\mathbf{S}_{1} & \mathbf{a}_{1}\mathbf{C}_{1} \\ \mathbf{S}_{1} & 0 & \mathbf{C}_{1} & \mathbf{a}_{1}\mathbf{S}_{1} \\ 0 & -1 & 0 & \mathbf{d}_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ \mathbf{T}_{1}^{2} &= \begin{bmatrix} \mathbf{C}_{2} & -\mathbf{S}_{2} & 0 & \mathbf{a}_{2}\mathbf{C}_{2} \\ \mathbf{S}_{2} & \mathbf{C}_{2} & 0 & \mathbf{a}_{2}\mathbf{S}_{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \\ \mathbf{T}_{2}^{3} &= \begin{bmatrix} \mathbf{C}_{3} & 0 & \mathbf{S}_{3} & 0 \\ \mathbf{S}_{3} & 0 & -\mathbf{C}_{3} & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ \mathbf{T}_{3}^{4} &= \begin{bmatrix} \mathbf{C}_{4} & 0 & -\mathbf{S}_{4} & 0 \\ \mathbf{S}_{4} & 0 & \mathbf{C}_{4} & 0 \\ 0 & -1 & 0 & \mathbf{d}_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ \mathbf{T}_{4}^{5} &= \begin{bmatrix} \mathbf{C}_{5} & 0 & \mathbf{S}_{5} & 0 \\ \mathbf{S}_{5} & 0 & -\mathbf{C}_{5} & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ \mathbf{T}_{5}^{6} &= \begin{bmatrix} \mathbf{C}_{6} & \mathbf{S}_{6} & 0 & 0 \\ \mathbf{S}_{6} & -\mathbf{C}_{6} & 0 & 0 \\ 0 & 0 & -1 & \mathbf{d}_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{split}$$

The total transformation between the base of the robot and the tool is

T _t	$a_{ase}^{tool} = 7$	$T_0^1 T_1^2 T_2^3 T_2^3$	$T_3^4 T_4^5 T_5^6$	
	$\int n_x$	O _x	a _x	p_x
	n _y	Oy	a _y	p _y
	n _z	Oz	a _z	p _z
	0	0	0	1

Where

$$n_{x} = C_{1}C_{23}(C_{4}C_{5}C_{6} - S_{4}S_{6}) - S_{1}(S_{4}C_{5}C_{6} + C_{4}S_{6}) - S_{5}C_{6}C_{1}S_{23}$$

 $n_{y} = S_{1}C_{23}(C_{4}C_{5}C_{6} - S_{4}S_{6}) - S_{5}C_{6}S_{1}S_{23}$ $+C_{1}(S_{4}C_{5}C_{6}+C_{4}S_{6})$ $n_z = -S_{23}(C_4C_5C_6 - S_4S_6)$ $-S_5C_6C_{23}$ $o_x = C_1 C_{23} (C_4 C_5 S_6 + S_4 C_6)$ $-S_1(S_4C_5S_6-C_4C_6)-S_5S_6C_1S_{23}$ $o_{v} = S_{1}C_{23}(C_{4}C_{5}S_{6} + S_{4}C_{6})$ $+C_1(S_4C_5S_6 - C_4C_6)$ $-S_1S_{23}S_5S_6$ $o_z = (C_4 C_5 S_6 + S_4 C_6)(-S_{23})$ $-S_5S_6C_{23}$ $a_x = C_1 C_{23} (-C_4 S_5) + S_1 S_4 S_5)$ $-C_5C_1S_{23}$ $a_{v} = S_{1}C_{23}(-C_{4}S_{5}) - C_{1}S_{4}S_{5}$ $-C_5S_1S_{23}$ $a_{z} = S_{23}C_{4}S_{5} - C_{5}C_{23}$ $p_x = C_1 C_{23} C_4 S_5 d_6 - S_1 S_4 S_5 d_6$ $+C_{1}S_{23}(C_{5}d_{6}+d_{4})$ $+a_{2}C_{1}C_{2} + a_{1}C_{1}$ $p_{y} = C_4 S_5 d_6 S_1 C_{23} + C_1 S_4 S_5 d_6$ $+(C_5d_6+d_4)S_1S_{23}$ $+a_{2}S_{1}C_{2} + a_{1}S_{1}$ $p_{z} = -S_{23}C_{4}S_{5}d_{6}$ $+C_{23}(C_5d_6+d_4)-a_2S_2+d_1$

At home - position

$$\theta_1 = 0^0, \theta_2 = -90^0, \theta_3 = 0^0$$

 $\theta_4 = 0^0, \theta_5 = 0^0, \theta_6 = 0^0$

So, at home position:

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$$T_{\text{base}}^{\text{tool}} = \begin{bmatrix} 0 & 0 & +1 & -(d_4 + d_6) + a_1 \\ 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & d_1 + a_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
Thus

Thus

$$x^{\circ} = z^{\circ}$$
$$y^{0} = -y^{6}$$
$$z^{0} = x^{6}$$

6

Which is verified by the Figure 3(a) and Figure 3(g)

III. Experimental Set-Up

In our experimental set up we have tried to find the reliability of the robot in terms of its performance. The flowchart for calculating reliability is given in Appendix A. To perform experiment on an industrial 6-axes KUKA robot, the following three steps are prerequisite:

- 1. Mastering of robot.
- 2. Tool Calibration
- 3. Base Calibration

In order to find reliability the following procedure is used :

- 1. The mastering of robot is done with the help of EMT.
- 2. The tool calibration of the robot is done by XYZ 4 point method.
- 3. Activate the tool by programming.
- 4. The base calibration of the robot is done by "3 point" method.
- 5. Activate the base by programming (Ex Base 7).
- 6. The robot is now programmed and moved to a point (the centre of a circle) in base 7 as shown in Figure 4 and Figure 5.

The tool is brought from home position to the centre of the circle in accordance with the programme given in Appendix B. The experiment is performed at 75% of the rated speed (2m/sec) and 40,000 observation are taken. The time taken to perform the experiment is 13 hours 20 minutes.

IV. Observations and Results

The robot is intercepted for once in total number of observations. So reliability is calculated as follows:

$$R = \frac{N_s}{N}$$

$$=\frac{39999}{40000}=.999$$

V. Conclusion

The given repeatability of the KR-16 robot is \pm .05 mm and the calculated reliability of this robot is .999. We conclude that high value of repeatability or low repeatability index ensures high reliability.



Fig.1-Axes KUKA Robot



Fig.2: Dimensions of 6 Axes KUKA Robot



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Fig. 3(d)







Fig. 3(f)











Fig.5

References

- [1] Zhang Kai, Liu Chengliang, Fu-Zhuong, "Track Planning of 6R Robot and its Application to Welding", Journal of Machine Design, Tianjin, China, Oct-2002, pp. 20-23.
- [2] Luo Jiajia, Hu Guoqing, "Study on the Simulation of Robot Motion based on MAT LAB", Journal of Xiamin University, China, Sept-2005, pp. 640-644.
- [3] Dhillan, B. S., and Yang, N., "Reliability Analysis of a Repairable Robot System", Journal of Quality in Maintenance Engineering, Vol. 2, No. 2, 1996, pp. 30-37.

- [4] Dhillan, B. S.,, "Robot Reliability and Safety", Springer-Verlag, New York, 1991.
- [5] Korayem, M. H., and Iravani, A.,"Improvement of 3P and 6R Mechanical Robot Reliability and Quality applying FMEA and QFD Approaches", Journal of Robotics and Computer-Integrated Manufacturing, Vol. 24, 2008, pp. 472-487.
- [6] McInroy, J.E., and Saridis, G. N., "Reliability Analysis in Intelligent Machines", IEEE Transactions on Systems, Man and Cybernetics, July-1990, pp. 1402-1407.
- [7] Smith, R., and Gini, M., "Reliable Real Time Robot Operation Employing Intelligent Forward Recovery", Journal of Robotic Systems, Vol. 3, No. 3, 1986, pp. 281-300.
- [8] Paul, R. P., and Stevenson, C. N., "Kinematics of Robot Wrists", International Journal of Robotics Res., Vol. 2, No.1, 1983, pp. 31-38.
- [9] 6-Axis Robot-free-cad [online]: www.sourceForge.net
- [10] Hirai, K., Hirose, M., Haikawa, Y. "The Development of Honda Humanoid Robot", IEEE International Conference on Robotics and Automation, 1998, pp. 1321-1326.
- [11] KUKA Robotics Corporation [online]: http://www.kuka-robotics.com/
- [12] Dahari Mahidzal, Tan Jian-Ding, "Forward and Inverse Kinematics Models for Robotic Welding Process Using KR-16KS KUKA Robot", IEEE International Conf. on ,Simulation and Optimization, Kuala Lumpur, 2011, pp. 1-6.
- [13] Wen Guojun; Xu Linhong; He Fulun, "Offline Kinematics Simulation of 6-DOF Welding Robot", IEEE/ICMTMA, International Conf. on Measuring Technology and Mechtronics Automation, 2009, pp. 283-286.
- [14] Bhatti, P.K.; Rao S.S., "Reliability analysis of robot manipulators", Proc. Of the ASME on Design Automation Conference, Boston, 1987, pp. 45-53.
- [15] Gordon J.W., Curry J.J., "Reliability analysis of the RRV-1 robot", Proc. of 33rd Conference on remote systems technology, lagrage park, 1987, pp- 210 – 214.



Where R=Reliability, N_s =Number of successful experiments and N=Total number of experiments

APPENDIX- B

Program

1	DEF Vinay ()
2	INI
3	
4	PTP HOME Vel=100% DEFAULT
5	
6	PTP P1 Vel =100% PDAT1 Tool[7]:ymca Base [7]: nicebase
7	Loop
8	PTP P2 CONT Vel =100% PDAT2 Tool[7]:ymca Base [7]: nicebase
9	LIN P3 Vel =2 m/s CPDAT1 Tool[7]:ymca Base [7]: nicebase
10	
11	LIN P2 CONT Vel =2 m/s CPDAT2 Tool[7]:ymca Base [7]: nicebase
12	PTP P1 CONT Vel =100% PDAT4 Tool[7]:ymca Base [7]: nicebase
13	Endloop
14	PTP HOME Vel=100% DEFAULT
15	
16	END